

# Simulation Study on the Concept of Lifetime-Equivalent Defect Density in the Context of Light-Induced Degradation (LID) Experiments

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**Abstract** — The concept of lifetime-equivalent defect density in the context of light-induced degradation investigation is evaluated by means of simulations especially in cases where more than one defect species changes over time. The superposition of boron-oxygen related light-induced degradation (BO-LID) with light- and elevated temperature-induced degradation (LeTID) as well as FeB dissociation as found in reality is discussed. Furthermore, the effect of varying background lifetime, as often encountered in the context of LeTID in mc-Si, and varying Fe density is studied.

**Index Terms** — defect kinetics, LID, BO-LID, LeTID, FeB

## I. INTRODUCTION

In many studies on defect formation and especially in the context of light-induced degradation (LID), *e.g.* [1]-[12], defect dynamics are studied using the synonymous quantity "effective, normalized, relative or lifetime-equivalent defect density  $\Delta N_{\text{leq}}$ "

$$\Delta N_{\text{leq}} := \frac{1}{\tau_{\text{eff}}(t)} - \frac{1}{\tau_{\text{eff}}(t_0)} = \frac{1}{f} \cdot \Delta N_{\text{SRH}} \quad (1)$$

where  $\tau_{\text{eff}}(t)$  is the effective excess charge carrier lifetime changing over time  $t$  and  $\tau_{\text{eff}}(t_0)$  is used as a reference at a certain point in time  $t_0$ . This lifetime-equivalent defect density  $\Delta N_{\text{leq}}$ , given in units of  $[\text{s}^{-1}]$  and not as the term "density" might imply in units of  $[\text{cm}^{-3}]$ , has proven to be a valuable quantity because it is directly proportional to the change in actual defect density  $N_{\text{SRH}}$  of a single bulk defect species with its lifetime given, *e.g.*, by Shockley-Read and Hall's (SRH) theory [13], [14] as

$$\frac{1}{\tau_{\text{SRH}}} = \frac{(n_0 + p_0 + \Delta n)}{\frac{n_0 + \Delta n + n_1}{\sigma_p v_{\text{th},p}} + \frac{p_0 + \Delta n + p_1}{\sigma_n v_{\text{th},n}}} \cdot N_{\text{SRH}} = \frac{1}{f} \cdot N_{\text{SRH}} \quad (2)$$

because taking the difference of inverse effective lifetimes comprising multiple recombination channels

$$\frac{1}{\tau_{\text{eff}}} = \frac{1}{\tau_{\text{int}}} + \frac{1}{\tau_{\text{surface}}} + \sum_j \frac{1}{\tau_{\text{SRH},j}} \quad (3)$$

cancels out any lifetime component not variable in time, be it surface, intrinsic or bulk (SRH) defect related. A more detailed derivation of  $\Delta N_{\text{leq}}$  and its properties can be found in [15].

However, it should be noted that (i)  $\Delta N_{\text{leq}}$  (like  $\tau_{\text{SRH}}$ ) depends specifically on injection  $\Delta n$  via the pre-factor  $f(\Delta n)$  defined in Eq. 2, (ii)  $\Delta N_{\text{leq}}$  only depicts the change in  $N_{\text{SRH}}$  occurring from  $t_0$  to  $t$  and not absolute  $N_{\text{SRH}}$ , and (iii) Eq. 1 describes the change of only one defect. If a multitude of  $j$  different defects changes in parallel, Eq. 1 expands to

$$\Delta N_{\text{leq}} = \sum_j \frac{1}{f_j} \cdot \Delta N_j = \sum_j \Delta N_{\text{leq},j} \quad (4)$$

and  $\Delta N_{\text{leq}}$  corresponds to an  $f_j$ -weighed sum of individually changing defect densities  $\Delta N_j$ .

In the following, different scenarios are studied by means of simulations demonstrating that  $\Delta N_{\text{leq}}$  can offer insights in defect dynamics but is also prone to misinterpretation.

## II. SIMULATION DETAILS

Three different defect types shall be discussed in the following: (i) a deep defect with  $\tau_n = 50 \mu\text{s}$  and  $\tau_p/\tau_n = 10$  which resembles the defect species responsible for boron-oxygen related light-induced degradation (BO-LID) [2], [6]; (ii) a deep defect with  $\tau_n = 35 \mu\text{s}$  and  $\tau_p/\tau_n = 30$  which resembles the defect species responsible for light- and elevated temperature-induced degradation (LeTID) [9], [16]-[19]; and (iii) iron at a density of  $5 \cdot 10^{10} \text{cm}^{-3}$  which prefers either to form FeB pairs with boron at room temperature in darkness, or to sit in an interstitial site at elevated temperatures and/or excess charge carrier injection [20]-[23]. The association or dissociation of these FeB pairs is assumed to occur completely. Apart from these defect types, effective lifetime  $\tau_{\text{eff}}$  is considered to be only limited by intrinsic or surface-related recombination. The latter one is parametrized in terms of a  $J_0$  model with  $J_0 = 15 \text{fA/cm}^2$  (per side) [24]. However, as both are assumed constant, they cancel out anyway when  $\Delta N_{\text{leq}}$  is calculated. Figures 1 and 2 depict the lifetime components of those defects in p-type material (doping  $p_0 = 1 \cdot 10^{16} \text{cm}^{-3}$ ) and the resulting effective lifetime in the injection range typically used in lifetime studies using the photoconductance decay method.

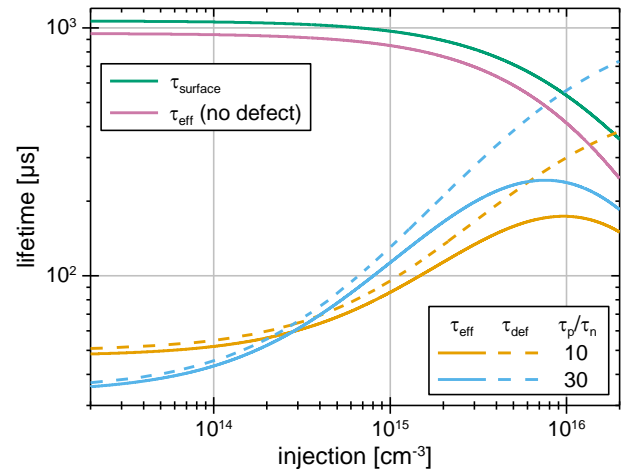


Fig. 1. Injection-dependent lifetime components  $\tau_{\text{def}}$  of the first two defect species as well as effective lifetime  $\tau_{\text{eff}}$  resulting from the superposition of the respective defect species with intrinsic and surface recombination. ( $T = 300 \text{K}$ ,  $p_0 = 1 \cdot 10^{16} \text{cm}^{-3}$ )

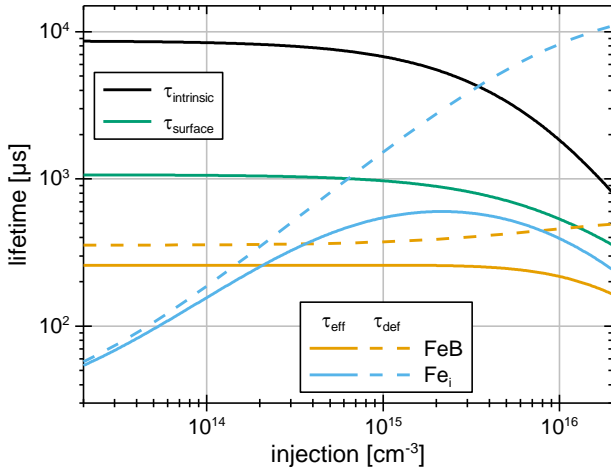


Fig. 2. Injection-dependent lifetime components  $\tau_{\text{def}}$  of FeB and  $\text{Fe}_i$  as well as effective lifetime  $\tau_{\text{eff}}$  resulting from the superposition with intrinsic and surface recombination. ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

The strong difference in carrier capture cross-sections of FeB ( $\sigma_p = 5 \cdot 10^{-15} \text{ cm}^2$ ,  $\sigma_n = 3 \cdot 10^{-15} \text{ cm}^2$ ) and  $\text{Fe}_i$  ( $\sigma_p = 7 \cdot 10^{-17} \text{ cm}^2$ ,  $\sigma_n = 4 \cdot 10^{-14} \text{ cm}^2$ ) results in a characteristic cross-over point (cop) of the lifetime curves at  $\Delta n_{\text{cop}} \sim 2 \cdot 10^{14} \text{ cm}^{-3}$  [20]-[23]. This characteristic behavior of iron allows for a comparatively easy quantification of iron in silicon by intentionally switching iron between those states by illumination (FeB dissociation) and dark storage at room temperature (FeB association). However, unintentional dissociation after dark storage is a nuisance during light-induced degradation studies.

Figure 3 shows the lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  determined from the lifetime data in Fig. 1 using the defect-free effective lifetime  $\tau_{\text{eff,nodef}}$  as reference and from  $\tau_{\text{eff,Fe}}$  in Fig. 2 using the associated state (FeB) as reference. It should be noted that the  $\tau_p/\tau_n$  ratio translates directly from  $\tau_{\text{SRH}}$  to  $\Delta N_{\text{leq}}$  and thus  $\Delta N_{\text{leq}}$  strongly increases for decreasing injection for deep defects. It is therefore important to state always the injection at which  $\Delta N_{\text{leq}}$  was determined together with substrate doping  $p_0$  because  $\tau_{\text{SRH}}$  (Eq. 2) shifts with injection relative to  $p_0$ .

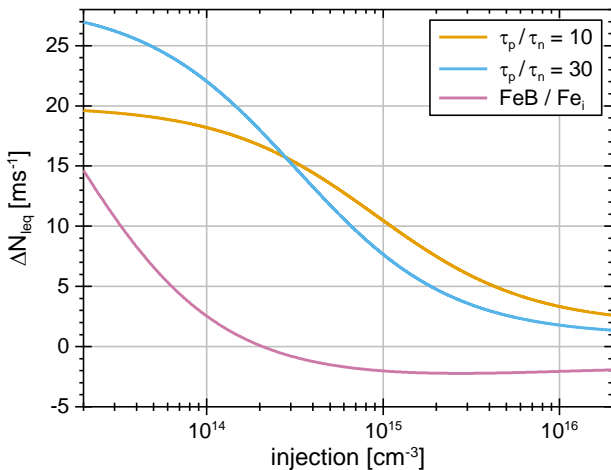


Fig. 3. Injection-dependent lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  determined from Figs. 1 and 2. ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

Describing the dissociation of FeB to  $\text{Fe}_i$  in terms of  $\Delta N_{\text{leq}}$  yields at first glance a counter-intuitive behavior of  $\Delta N_{\text{leq}}$ . While  $\Delta N_{\text{leq}}$  is positive below the cross-over point and one would conclude that defects have formed, it becomes negative above the cross-over point and one would conclude that defects have vanished even though total iron concentration has of course not changed. Whether the FeB pairs completely dissociate or not, is irrelevant here because the influence of still associated FeB pairs cancels out when  $\Delta N_{\text{leq}}$  is calculated.

### III. SIMULATED DEFECT DYNAMICS

Three different scenarios are presented in the following. In a first *scenario A*, that shall resemble BO-LID, a single defect species forms and vanishes over the course of time. In a second *scenario B*, a second defect species, that shall resemble LeTID, forms and vanishes in parallel to the first defect species (extending *scenario A*). In a third *scenario C*, the dynamic of these two defect species is superimposed with the dissociation of FeB (extending *scenario B*). The increase and subsequent decrease of respective defect densities  $N_x$  in *scenarios A & B* related to the two defect species, resulting in a degradation and regeneration of lifetime, is assumed to follow the equation [25]

$$N_x(t) = -N_{1,x} \cdot \exp\left(-\frac{t}{t_{\text{deg},x}}\right) + N_{2,x} \cdot \exp\left(-\frac{t}{t_{\text{reg},x}}\right) \quad (5)$$

with  $t_{\text{deg}}$  and  $t_{\text{reg}}$  being characteristic time constants of the respective degradation and regeneration phase. For the FeB dissociation, a simple exponential decay

$$\frac{[\text{Fe}_i]}{[\text{Fe}]_{\text{total}}} = 1 - \frac{[\text{FeB}]}{[\text{Fe}]_{\text{total}}} = 1 - \exp\left(-\frac{t}{t_{\text{Fe}}}\right) \quad (6)$$

with time constant  $t_{\text{Fe}}$  is assumed. As it is not the intention of this paper to depict a specific situation but rather to describe the general behavior, time  $t$  is treated as a dimensionless quantity. Thus only relative but not absolute time constants are relevant.

#### A. Scenario A: BO-LID

Boron-doped, oxygen-rich silicon (*e.g.* Cz-Si) is prone to the formation of a recombination-active defect species under excess charge carrier injection (*e.g.* by illumination) at low temperatures ( $< 100^\circ\text{C}$ ) resulting in a degradation of lifetime [2], [6]. However, it is also observed that illuminated annealing at elevated temperatures ( $> 50^\circ\text{C}$ ) can lead to a subsequent deactivation of the harmful defect species resulting in a slow regeneration of lifetime [25], [26]. Within this scenario, the fast degradation and slow regeneration are accounted for by using  $t_{\text{deg,BOLID}} = 2.5$  and  $t_{\text{reg,BOLID}} = 25$ . Under the correct conditions, lifetime recovery can be almost complete [25] and therefore it is assumed here that  $N_{1,\text{BOLID}} = N_{2,\text{BOLID}}$ . Furthermore, it is assumed that the low injection lifetime of BO-LID drops to  $\tau_n = 50 \mu\text{s}$  at maximum defect density (maximum of Eq. 5) and injection dependence is well described by  $\tau_p/\tau_n = 10$  [2], [6]. This scenario could, *e.g.*, occur during illuminated annealing at a temperature of  $75^\circ\text{C}$  and 1 sun illumination intensity [27].

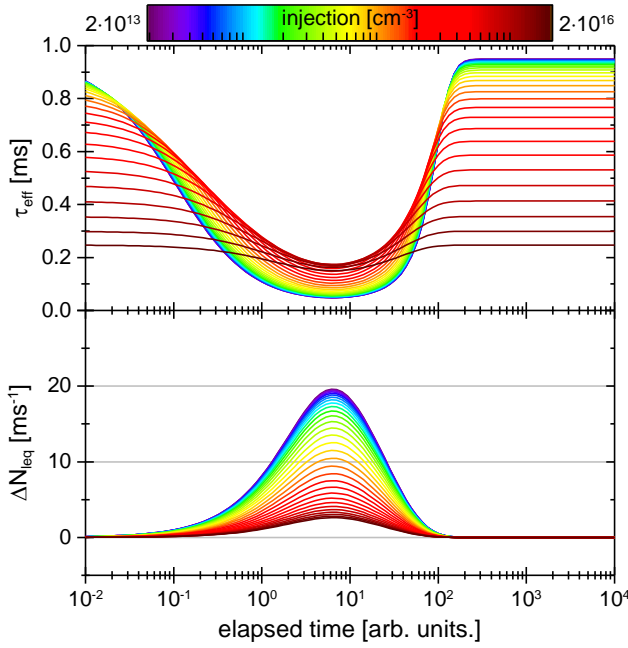


Fig. 4. Time-resolved evolution of the effective lifetime  $\tau_{\text{eff}}$  and derived lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  at various color-coded injection levels  $\Delta n$  in *scenario A*. ( $T = 300$  K,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

The simulation results of *scenario A* are shown in Fig. 4. In the short and long term, when BO-LID degradation has not yet kicked-in or regeneration is already almost complete,  $\tau_{\text{eff}}$  is limited by surface-related recombination (see Fig. 1) and thus  $\tau_{\text{eff}}$  is almost injection-independent at low injection levels (violet to green colors) and decreases for high injection levels (yellow to red colors). In the medium term, BO-LID results in the expected inversion of the color order (being characteristic for a deep SRH defect) and the typical bathtub-like broad lifetime minimum at low injection becoming narrower at higher injection levels. Only after calculation of  $\Delta N_{\text{leq}}$  it becomes obvious that the various (injection) color-coded lines depict the same defect dynamic and yield the same time constants even though the amplitude differs (see Fig. 3).

### B. Scenario B: BO-LID and LeTID in parallel

Besides BO-LID, light- and elevated temperature-induced degradation (LeTID) [7]-[11], [16]-[19] seems to occur in Cz-Si as well [8], [12]. Like BO-LID, LeTID features not only a degradation but also a regeneration phase. Whether describing LeTID by Eq. 5 is perfectly correct or not is irrelevant here as the exact progression with time does not matter. At least at low temperatures (*e.g.*  $75^\circ\text{C}$ ), both degradation and regeneration of lifetime due to LeTID occur on a longer time scale compared to BO-LID, however, some overlap occurs. Therefore, time constants of LeTID in *scenario B* are chosen to  $t_{\text{deg,LeTID}} = 25$  and  $t_{\text{reg,LeTID}} = 250$ . Under the correct conditions, lifetime recovery seems to be almost complete and therefore it is assumed here that  $N_{1,\text{LeTID}} = N_{2,\text{LeTID}}$ . However, one should note that this might be a critical assumption in reality. Furthermore,

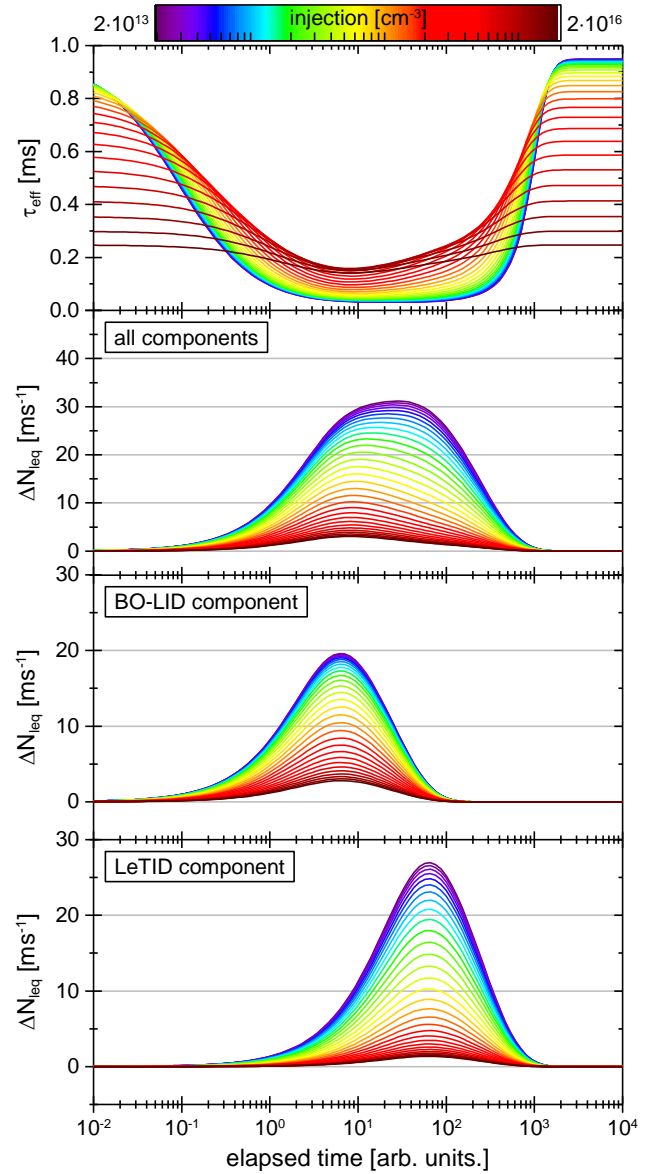


Fig. 5. Time-resolved evolution of the effective lifetime  $\tau_{\text{eff}}$  and derived lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  (in total and for BO-LID and LeTID separately) at various color-coded injection levels  $\Delta n$  in *scenario B*. ( $T = 300$  K,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

it is assumed that the low injection lifetime of LeTID drops to  $\tau_n = 35 \mu\text{s}$  at maximum defect density and injection dependence is well described by  $\tau_p/\tau_n = 30$  [19]. This *scenario B* could just like *scenario A*, *e.g.*, occur during illuminated annealing at a temperature of  $75^\circ\text{C}$  and 1 sun illumination intensity [27].

Figure 5 shows the simulation results of *scenario B*. The first thing to note is the broadening of the bathtub-like minimum in effective lifetime which, of course, results from the slower onset and subsequent recovery from LeTID. At first glance, especially if  $\tau_{\text{eff}}$  and/or  $\Delta N_{\text{leq}}$  are evaluated at an injection level of  $\Delta n \sim 1 \cdot 10^{15} \text{ cm}^{-3}$  (orange), there is no clear second minimum visible and one might conclude that the slow recovery is, for whatever reason, simply due to a slow regeneration of BO-LID.

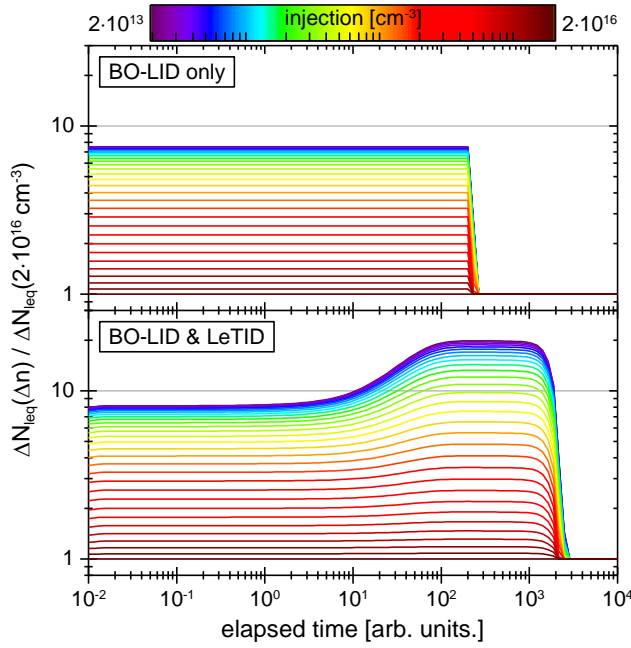


Fig. 6. Time-resolved evolution of the  $\Delta N_{\text{leq}}$  ratio relative to  $\Delta N_{\text{leq}}$  at  $\Delta n_{\text{max}} = 2 \cdot 10^{16} \text{ cm}^{-3}$  at various color-coded injection levels  $\Delta n$  in *scenarios A & B*. ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

However, already a closer look at  $\tau_{\text{eff}}(t)$  reveals a peculiar feature hardly compatible with single defect dynamics (see Fig. 4): the exact position of minimum lifetime shifts to longer times the lower the injection is. This feature can be seen even more clearly in total  $\Delta N_{\text{leq}}$  where the red curves (higher injection) already drop after  $t = 10^1$ , but the blue/violet curves (lower injection) remain constant or even increase, and it can be highlighted even more by plotting not only  $\Delta N_{\text{leq}}$  but rather the ratio of  $\Delta N_{\text{leq}}$  at different injection levels. This is exemplarily shown in Fig. 6 for both, *scenario A & B* with respect to  $\Delta n_{\text{max}} = 2 \cdot 10^{16} \text{ cm}^{-3}$  (being the highest available injection level). While the ratio remains perfectly constant over time for all injection levels in *scenario A* (Fig. 6 top), it changes characteristically in *scenario B* (Fig. 6 bottom) after  $t = 10^1$  as LeTID gradually becomes the dominant lifetime limiting factor. Eventually, the ratio stabilizes on a higher level being characteristic for LeTID when regeneration of BO-LID is almost complete. The higher  $\Delta N_{\text{leq}}$  ratio level is a consequence of the higher assumed  $\tau_p/\tau_n$  ratio of LeTID ( $\tau_p/\tau_n = 30$ ) compared to BOLID ( $\tau_p/\tau_n = 10$ ). The abrupt drop in Fig. 6 in long-term is an artifact due to limited calculation accuracy as infinitesimal small numbers are divided up there.

### C. Scenario C: BO-LID, LeTID & FeB dissociation in parallel

Unfortunately, iron is a common contaminant in silicon with an enormous impact on lifetime in p-type silicon even in small concentrations as can be seen in Fig. 2. And even more unfortunate, FeB pairs present after dark storage react to light- and temperature treatments typically used in light-induced degradation studies by dissolving/releasing  $\text{Fe}_i$  and thus the

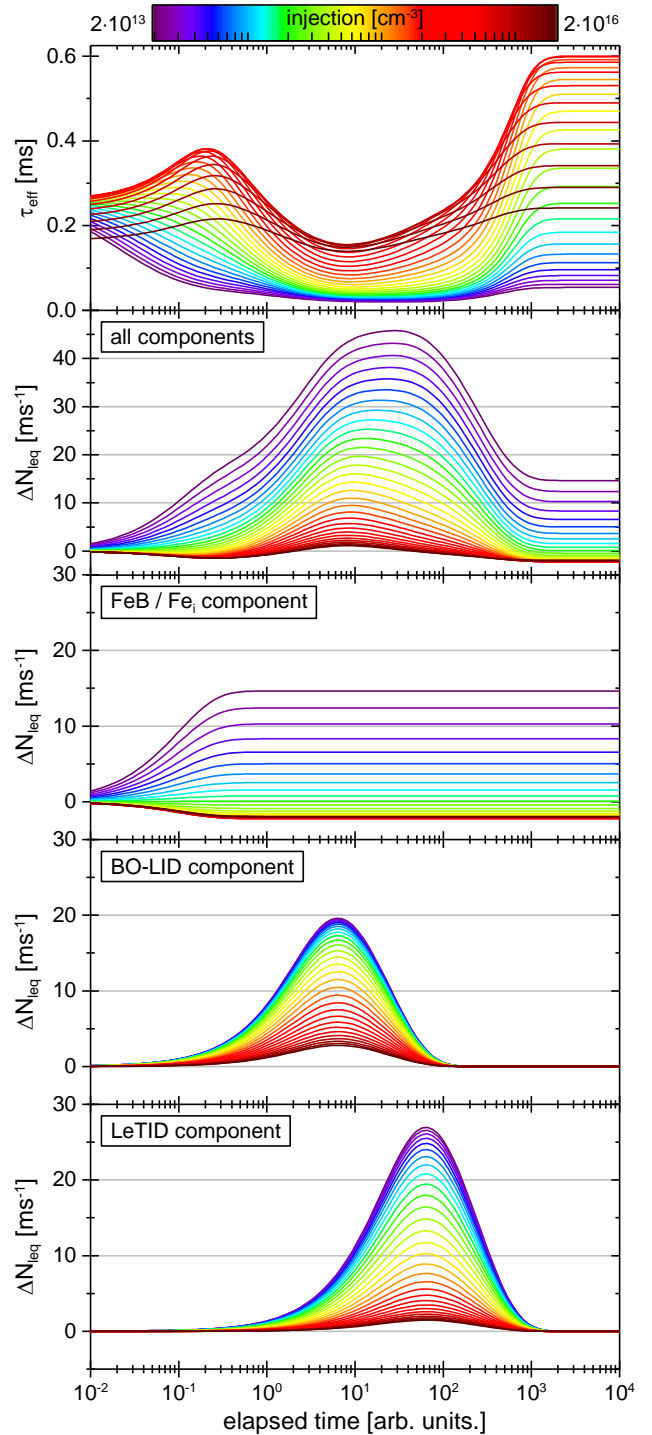


Fig. 7. Time-resolved evolution of the effective lifetime  $\tau_{\text{eff}}$  and derived lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  (in total and for FeB/ $\text{Fe}_i$ , BO-LID and LeTID separately) at various color-coded injection levels  $\Delta n$  in *scenario C*. ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

changing influence of iron does not cancel out when  $\Delta N_{\text{leq}}$  is calculated. FeB dissociation is accounted for in *scenario C* assuming initial FeB and  $\text{Fe}_i$  concentrations of  $5 \cdot 10^{10} \text{ cm}^{-3}$  and  $0 \text{ cm}^{-3}$ , respectively, and a decay constant of 0.1.

Figure 7 shows the simulation results of *scenario C*. As discussed in the context of Fig. 3, the dissociation of FeB pairs results in positive  $\Delta N_{\text{leq}}$  values below the cross-over point ( $\Delta n_{\text{cop}} \sim 2 \cdot 10^{14} \text{ cm}^{-3}$ ) and negative  $\Delta N_{\text{leq}}$  values above the cross-over point. In consequence, total  $\Delta N_{\text{leq}}$  is reduced at high injection levels (orange/red) and even turns temporarily and in long-term negative. In contrast, total  $\Delta N_{\text{leq}}$  is permanently increased for low injection levels (violet/blue). Even though the  $\Delta N_{\text{leq}}$  component of both, BO-LID and LeTID, vanishes in long-term, total  $\Delta N_{\text{leq}}$  does not except for  $\Delta n_{\text{cop}} \sim 2 \cdot 10^{14} \text{ cm}^{-3}$  (green) where the  $\Delta N_{\text{leq}}$  component vanishes anyway. Hence one could conclude that regeneration of either BO-LID or LeTID is incomplete if  $\Delta N_{\text{leq}}$  is evaluated at injection levels above the cross-over point or seems to be “more than complete” at injection levels above the cross-over-point. As the latter is maybe counter-intuitive, one could conclude as well that the sample was initially already degraded to some extent.

The iron dynamics related change of sign hampers the injection-dependent analysis analogous to Fig. 6 as well. Hence, it is highly advisable to suppress the influence of iron in light-induced degradation experiments as much as possible, *e.g.*, by using optimized gettering processes. Alternatively, preparing the FeB/Fe<sub>i</sub> subsystem to a well-defined state, *e.g.*, by either completely associating the FeB pairs (by sufficiently long dark storage at low temperature) or dissociating the FeB pairs (by intense illumination) for each lifetime measurement. If this is not possible, analyzing defect dynamics at an injection level close to the cross-over point at least minimizes the influence of iron.

## VI. EXAMPLES FOR MISINTERPRETATION

As discussed before, it is important to note that the lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  may strongly depend on injection  $\Delta n$ . Unfortunately, there is plenty of room for misinterpretations if injection dependency is ignored. The following two examples shall demonstrate this. *Scenario D* deals with varying background bulk lifetime in different grains in mc-Si in combination with LeTID. It is noteworthy that laterally inhomogeneous surface passivation quality on Cz-Si and FZ-Si would result in a similar situation. *Scenario E* deals with varying iron contamination in different grains of mc-Si in combination with the dissociation of FeB pairs.

### A. Scenario D: LeTID and varying background lifetimes

It is a common feature of mc-Si that contaminants and crystal defects are inhomogeneously distributed and that bulk lifetime varies from grain to grain, especially if a wafer originates from the brick edge. Consider the following situation: A first, “good” grain features an injection-independent background lifetime  $\tau_{\text{bg,good}}$  of 300  $\mu\text{s}$ . A second, “bad” grain features an injection-independent background lifetime  $\tau_{\text{bg,bad}}$  of only 33  $\mu\text{s}$ . Again, doping level  $p_0$  is chosen to  $1 \cdot 10^{16} \text{ cm}^{-3}$ . Effective lifetime  $\tau_{\text{eff}}$ , including surface- and intrinsic-related lifetime components

(see Fig. 2), of the two grains is shown in Fig. 8 (solid lines). In both grains, LeTID is assumed to occur with the same (lifetime-equivalent) defect density which corresponds to a fully injection-dependent LeTID-related lifetime component with  $\tau_{\text{LeTID}} = 100 \mu\text{s}$  at  $\Delta n = 1 \cdot 10^{15} \text{ cm}^{-3}$  (red line). Degraded effective lifetime  $\tau_{\text{eff,deg}}$  including the LeTID-related lifetime component is then given by the dashed lines.

As mc-Si is known to be laterally inhomogeneous, LID studies often rely on (lifetime-calibrated) photoluminescence imaging to quantify changes in local effective lifetime  $\tau_{\text{eff}}$ . In many cases, a constant volume generation rate  $G$  (excitation photon flux) is used implying a local (steady-state) injection

$$\Delta n = G \cdot \tau_{\text{eff}} \quad (7)$$

In principle, an injection gradient between adjacent regions would provoke a compensation current, but this shall be omitted here for the sake of simplicity. Assuming a constant photon flux equivalent to 1 sun, resulting in a volume generation rate  $G_0$  of  $1.25 \cdot 10^{19} \text{ cm}^{-3} \text{ s}^{-1}$ , yields the specific injection levels marked in Fig. 8 that are, of course, the lower, the lower the effective lifetime is.

A calculation of apparent  $\Delta N_{\text{leq}}$  values in each grain according to Eq. 1, completely ignoring that the individual  $\tau_{\text{eff}}$  was determined at different injection levels, yields the marked values in Fig. 8 (bottom) which clearly differ. Thus one would conclude that the bad grain suffers more from LeTID even though the extent of LeTID was chosen similarly in both grains – a clear misinterpretation simply because apparent  $\Delta N_{\text{leq}}$  was not determined at the same injection level.

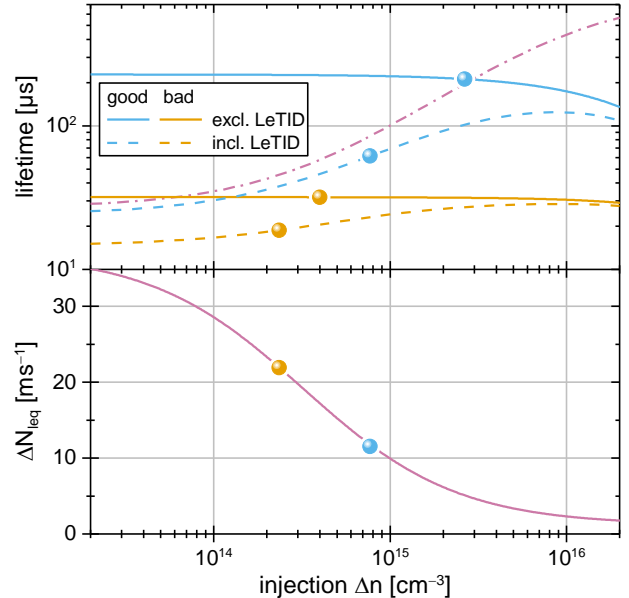


Fig. 8. (top) Injection-dependent effective lifetimes  $\tau_{\text{eff}}$  of the good and bad grain including LeTID (solid lines) and excluding LeTID (dashed lines) as well as the LeTID-related lifetime component (red dash-dotted line). Injection obtained under constant generation conditions is marked for each curve. (bottom) Lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  of LeTID and the apparent  $\Delta N_{\text{leq}}$  in the two grains. ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

### B. Scenario E: Inhomogeneous Fe distribution

It is a common feature in mc-Si as well that contaminants, like iron, are inhomogeneously distributed across a wafer [28], [29]. For example, in-diffusion from the crucible walls results in higher contaminant (iron) densities closer to the respective wafer edges. Consider the following scenario: A first, highly (hi) iron-contaminated grain initially features after dark storage  $[\text{FeB}]_{\text{hi}} = 5 \cdot 10^{11} \text{ cm}^{-3}$ . A second, lowly (lo) iron-contaminated grain features  $[\text{FeB}]_{\text{lo}} = 1 \cdot 10^{11} \text{ cm}^{-3}$ . Apart from  $\text{Fe}_i$  or  $\text{FeB}$ , only surface and intrinsic recombination (see Fig. 2) shall limit effective lifetime of the boron-doped p-type material ( $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ ). The effective lifetime curves in the two grains with iron being associated with or dissociated from boron are shown in Fig. 9. However, for the sake of discussion, the experimenter shall be unaware of this iron contamination while he applies illumination within a LID experiment starting after dark storage. Thus iron is in the  $\text{FeB}$  state during the first measurement and in the  $\text{Fe}_i$  state for later measurements.

As it was done in *scenario D*, local effective lifetimes  $\tau_{\text{eff}}$  are determined with a constant volume generation rate  $G$ . Figure 9 exemplarily illustrates the respective  $\tau_{\text{eff}}$  for  $G = \frac{1}{3} \cdot G_0$  as well. Again, ignoring that  $\tau_{\text{eff}}$  was determined at different injection levels, apparent  $\Delta N_{\text{leq}}$  due to the unexpected dissociation of  $\text{FeB}$  pairs is calculated for both grains in dependence of volume generation rate  $G$ . Figure 10 depicts the relation of apparent  $\Delta N_{\text{leq}}$  and generation for both grains and especially for the highlighted generation  $G = \frac{1}{3} \cdot G_0$ . As can be seen, apparent  $\Delta N_{\text{leq}}$  strongly depends on the choice of generation and on the iron contamination level. For  $G = \frac{1}{3} \cdot G_0$  ( $\frac{1}{3}$  sun) it looks, at first glance, as if local defect density has increased in the highly iron-contaminated grain due to applied illuminated annealing whereas it seems to have decreased in the lowly iron-contaminated grain. However, evaluation at  $G = 1 \cdot G_0$  (1 sun) yields a different result: here it appears that local defect density has decreased in both grains.

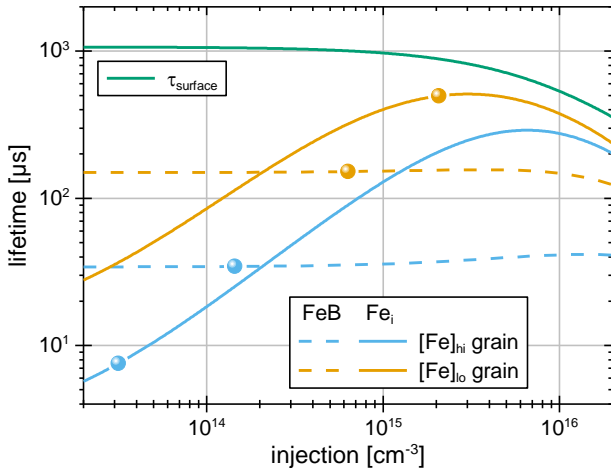


Fig. 9. Injection-dependent effective lifetimes  $\tau_{\text{eff}}$  of the highly and lowly iron-contaminated grain in the associated (dashed lines) and dissociated  $\text{FeB}$  state (solid lines). The points mark the injection obtained with a generation rate of  $\frac{1}{3} \cdot G_0$ . ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

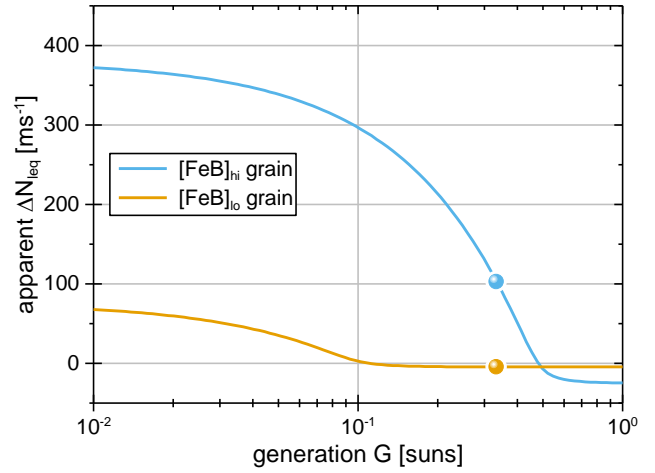


Fig. 10. Apparent lifetime-equivalent defect density  $\Delta N_{\text{leq}}$  in the highly and lowly iron-contaminated grain in dependence of normalized volume generation rate  $G$ . ( $T = 300 \text{ K}$ ,  $p_0 = 1 \cdot 10^{16} \text{ cm}^{-3}$ )

Again, the reason for this misinterpretation is due to ignoring injection dependence in combination with being unaware that the sample is iron-contaminated.

As long as obtained injection for a certain generation rate remains above the cross-over point of the  $\text{FeB}/\text{Fe}_i$  system, the  $\Delta N_{\text{leq}}$  ratio corresponds to the assumed initial  $[\text{FeB}]_{\text{hi}}/[\text{FeB}]_{\text{lo}}$  ratio of 5 in between the two grains even though apparent  $\Delta N_{\text{leq}}$  is negative. However, if injection drops below the cross-over point, which is easier to achieve for low  $\tau_{\text{eff}}$  due to high iron density,  $\Delta N_{\text{leq}}$  turns positive and then gradually increases with decreasing generation.

As can be seen from Fig. 10, there is a certain window in between  $\frac{1}{2} \cdot G_0$  and  $\frac{1}{10} \cdot G_0$ , where injection is already below the cross-over-point ( $\Delta n_{\text{cop}} \sim 2 \cdot 10^{14} \text{ cm}^{-3}$ ) in the highly iron-contaminated grain but still above it in the lowly iron-contaminated grain. The highlighted points for  $G = \frac{1}{3} \cdot G_0$  in Figs. 9 and 10 illustrate this situation.

## V. CONCLUSION

The lifetime-equivalent defect density  $\Delta N_{\text{leq}}$ , being a direct measure of changes in actual defect density in systems comprising only one changing defect species, can be a valuable approach for the quantification of defect dynamics.

However, in situations where more than one defect species is involved, total  $\Delta N_{\text{leq}}$  corresponds to the inseparable sum of individual  $\Delta N_{\text{leq}}$  components. But even then, the characteristic injection dependence of the individual  $\Delta N_{\text{leq}}$  components can be exploited to separate the individual defect species in light-induced degradation experiments, at least when the individual defect species exhibit differing kinetics.

In contrast, ignoring the specific injection dependence of  $\Delta N_{\text{leq}}$  can lead to serious misinterpretations as demonstrated in examples on LeTID and  $\text{FeB}$  dissociation.

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